
Optimisation in Aeronautics

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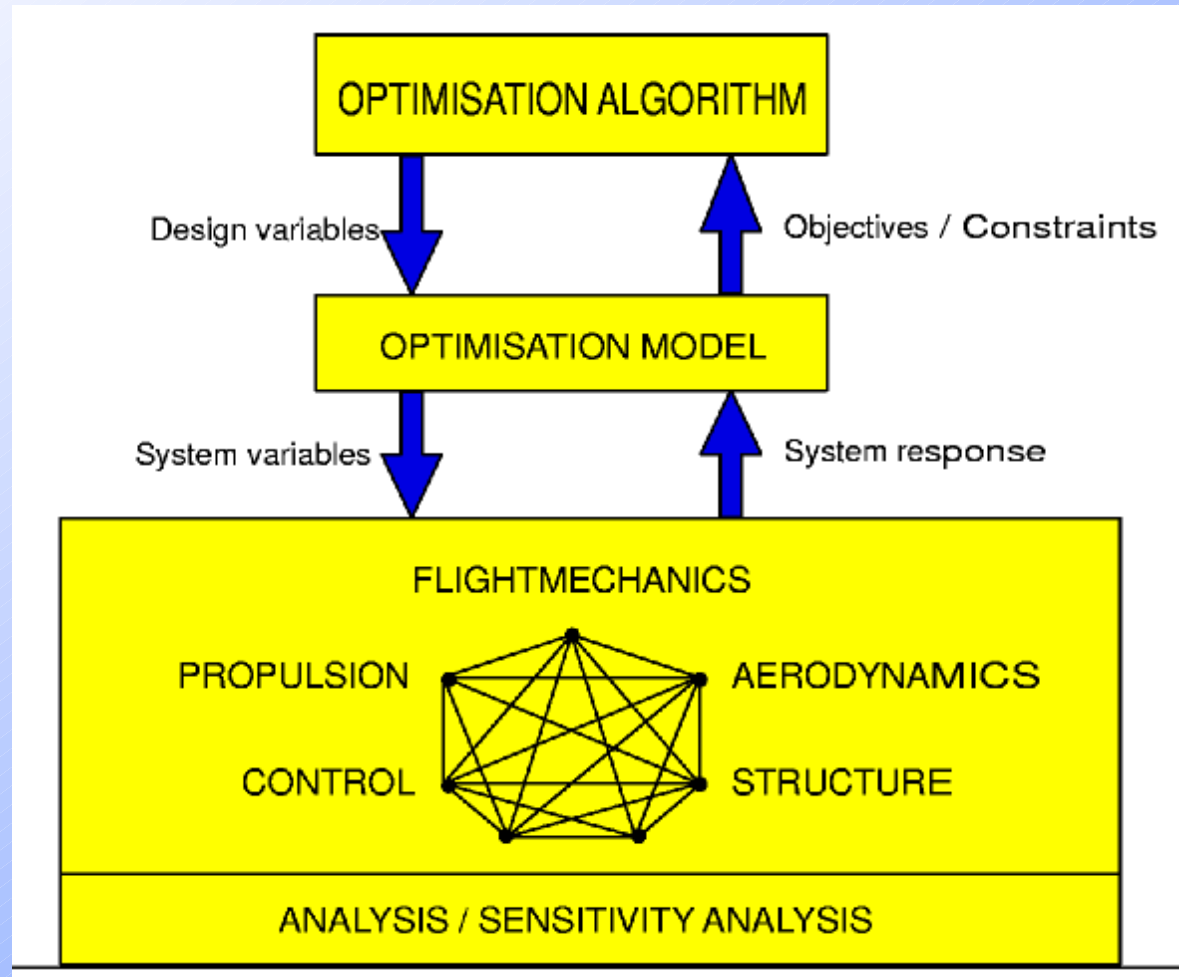
Part of this work was sponsored by the EU via the AEROSHAPE project

SUMMARY

- Aircraft design cycle
- Inverse two-point airfoil optimisation
- Drag reduction of RAE2822, a three-point optimisation challenge
- Supersonic commercial transport optimisation
- High Altitude Long Endurance (Hale) – Loiter time optimisation
- Why ‘Robust Design’ ?
- Conclusion

Optimisation in Aeronautics

Network of influences in aircraft design optimisation



Design network

2-point airfoil

Drag minimisation on RAE2822

SCT drag minimisation

Hale – Loiter time

Robust Design

Conclusions



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2-point (inverse?) airfoil design - Test Case Description

- Minimisation of an objective function which is the difference between computed/optimised pressure distribution at **two different design points with two pre-defined target pressures** (originally proposed by T. Labruyere, NLR)
- The objective function reads:

$$F(\alpha_1, \alpha_2, x(s), y(s)) = \sum_{n=1}^2 \left[W_n \int_0^1 \left(C_p^n(s) - C_{p,target}^n(s) \right)^2 ds \right]$$





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Two-point airfoil design - Test Case Description

Two different design conditions (i=1,2):

i=1: Typical high-lift airfoil at subsonic conditions

i=2: Typical high-speed airfoil at transonic conditions

Case	i=1	i=2
Ma	0.20	0.77
Re	5×10^6	10^7
Incidence	10.8°	1.0°
X_{trans}/c	0.03	0.03



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Inverse/two-point airfoil design - Numerical approach

Approach

- 2D (full) Navier-Stokes method
- Mesh resolution has been set to the lowest possible level (with respect to predictive accuracy) of 128x32 mesh points
- Computation time for one individual: < 60 sec. on 850MHz PC
- Parameterisation via Bezier Splines

First test on transonic case only

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Inverse airfoil design - GA results (64x16)



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Drag minimisation on RAE2822

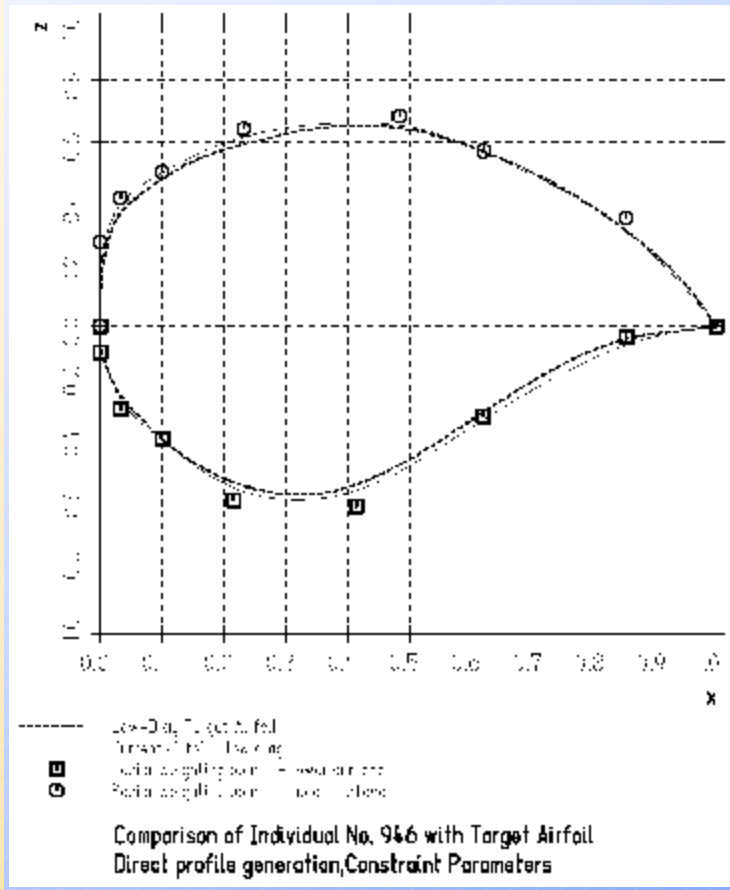
SCT drag minimisation

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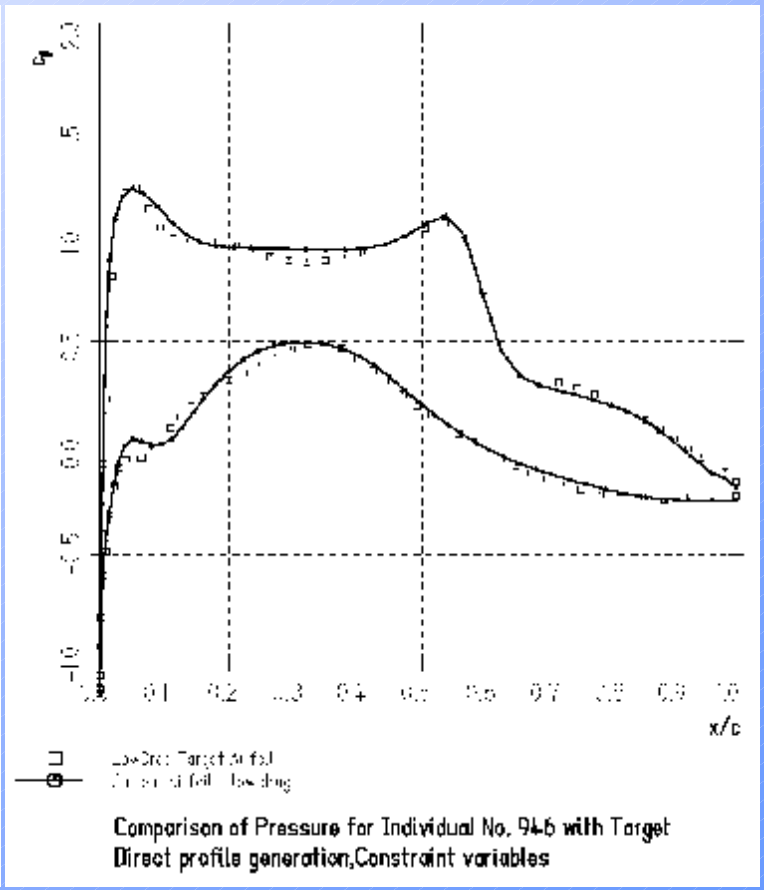
Robust Design

Conclusions

Shape



Pressure



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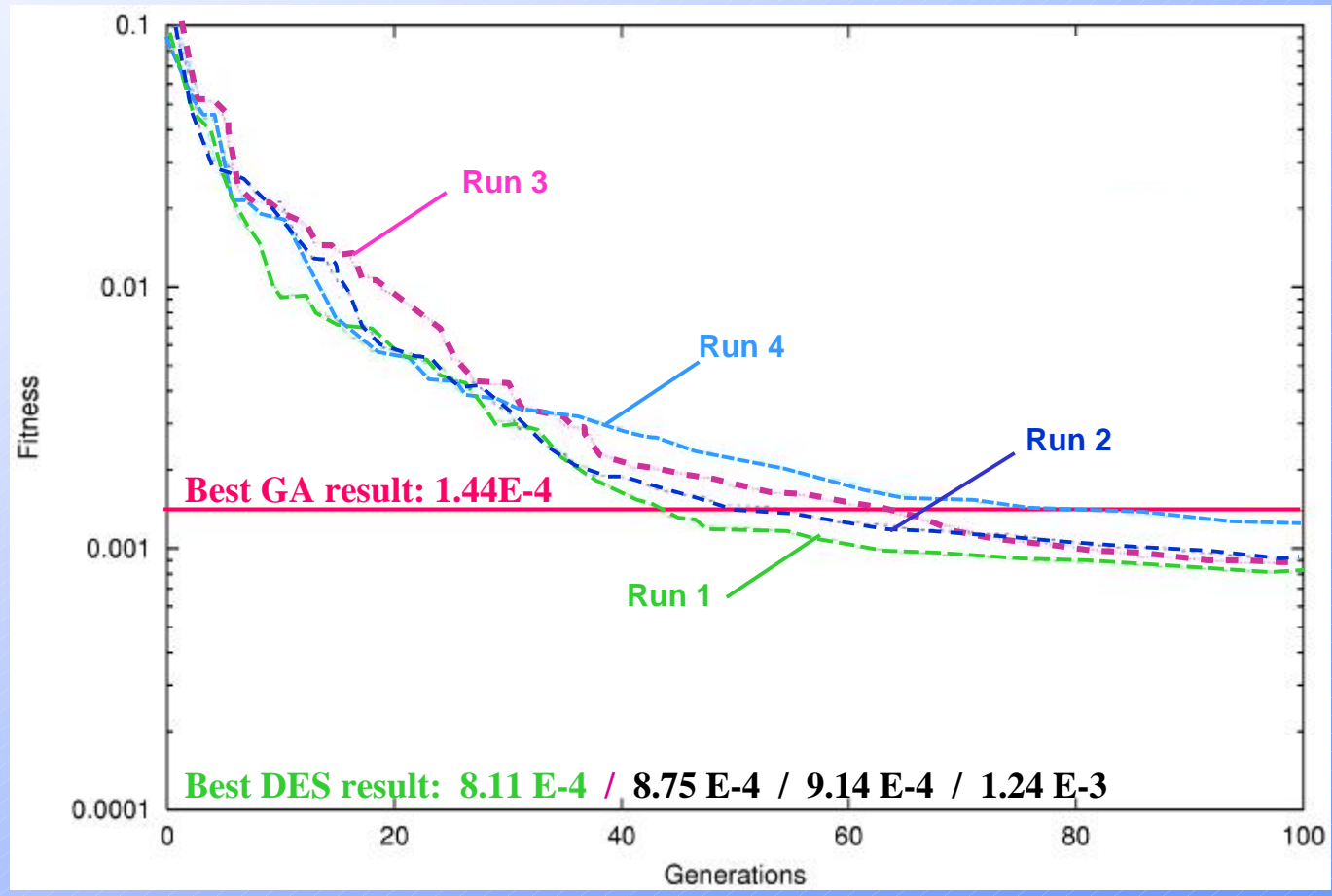
Hale – Loiter time

Robust Design

Conclusions

Inverse airfoil design - ES results by NUTECH

Strategy used: *DES, elitism incorporated*



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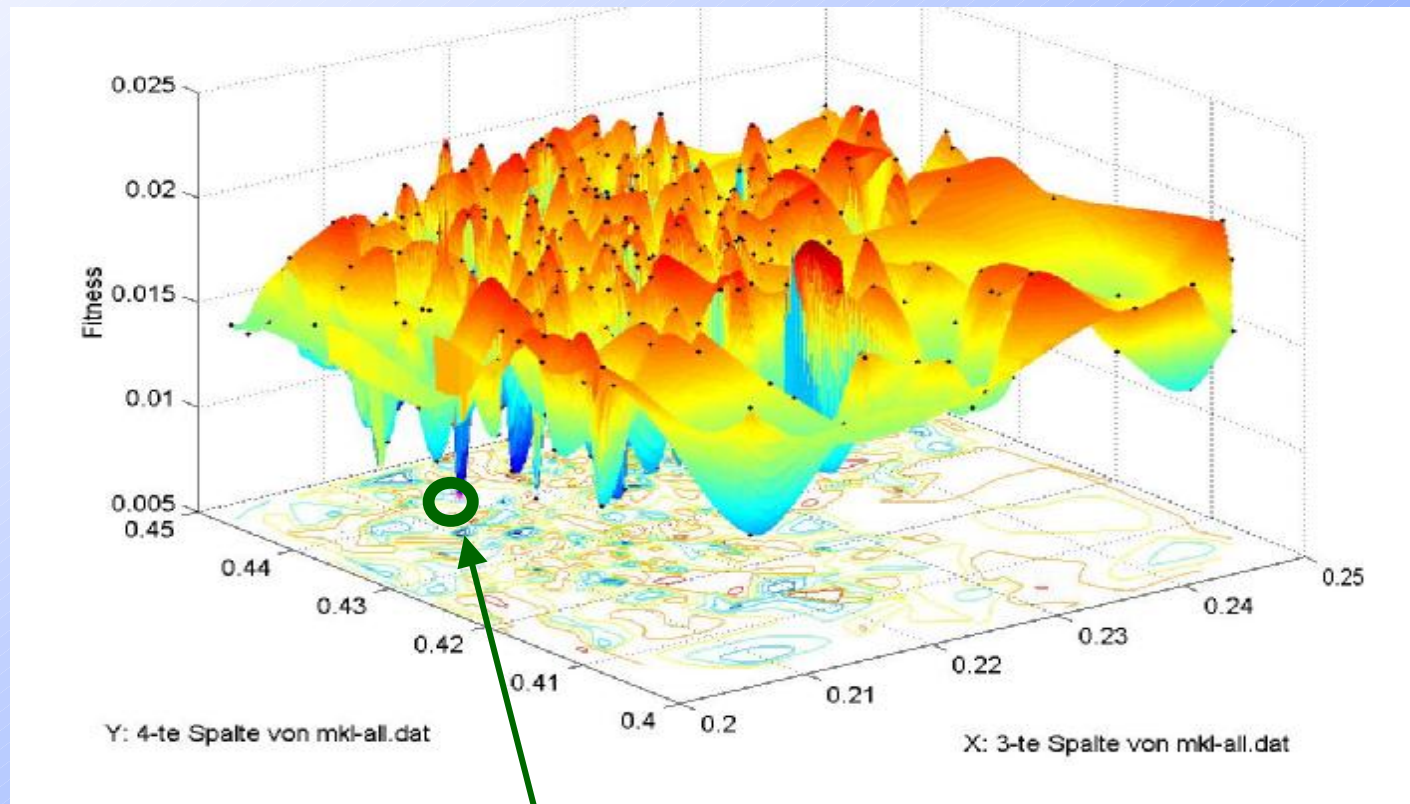
Hale – Loiter time

Robust Design

Conclusions

Inverse airfoil design - ES results by NUTECH

Fitness vs. first and second design parameter - low drag case



Optimum

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Two-point airfoil design - Parameterisation

Design network

2-point airfoil

Drag minimisation on RAE2822

SCT drag minimisation

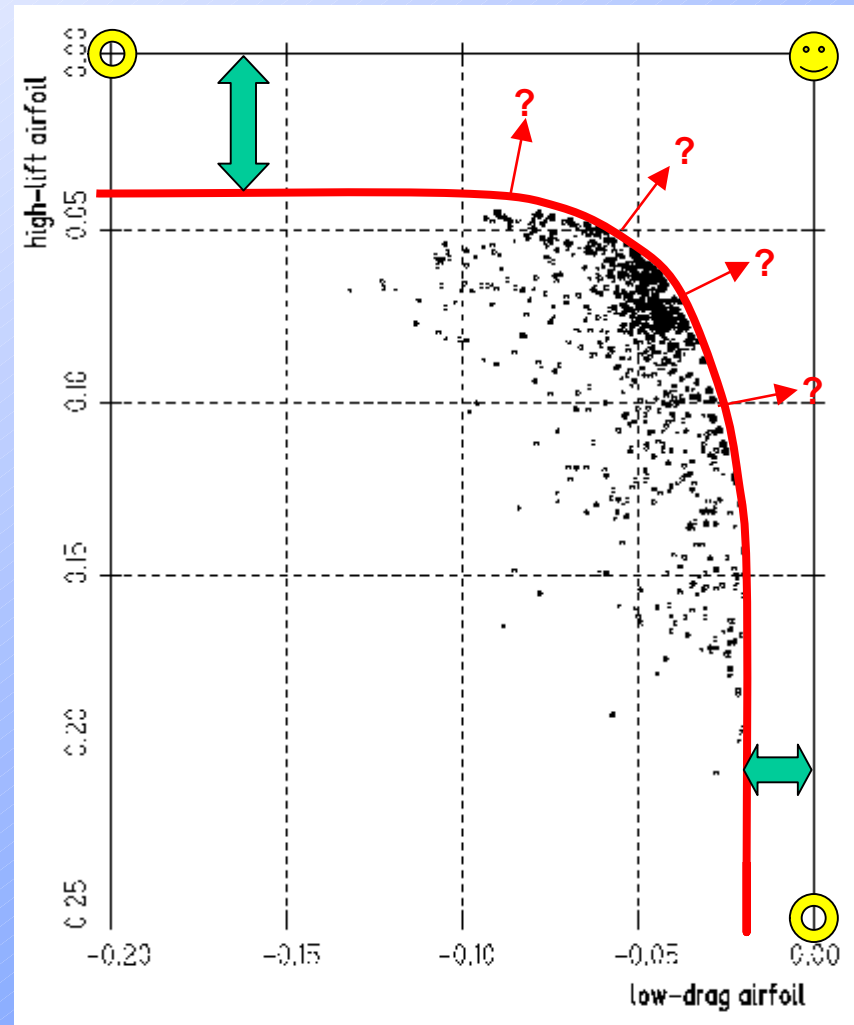
Hale - Loiter time

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Axes values:
Objective function =
Difference in pressure

**Pareto "gap" due to
Parameterisation**



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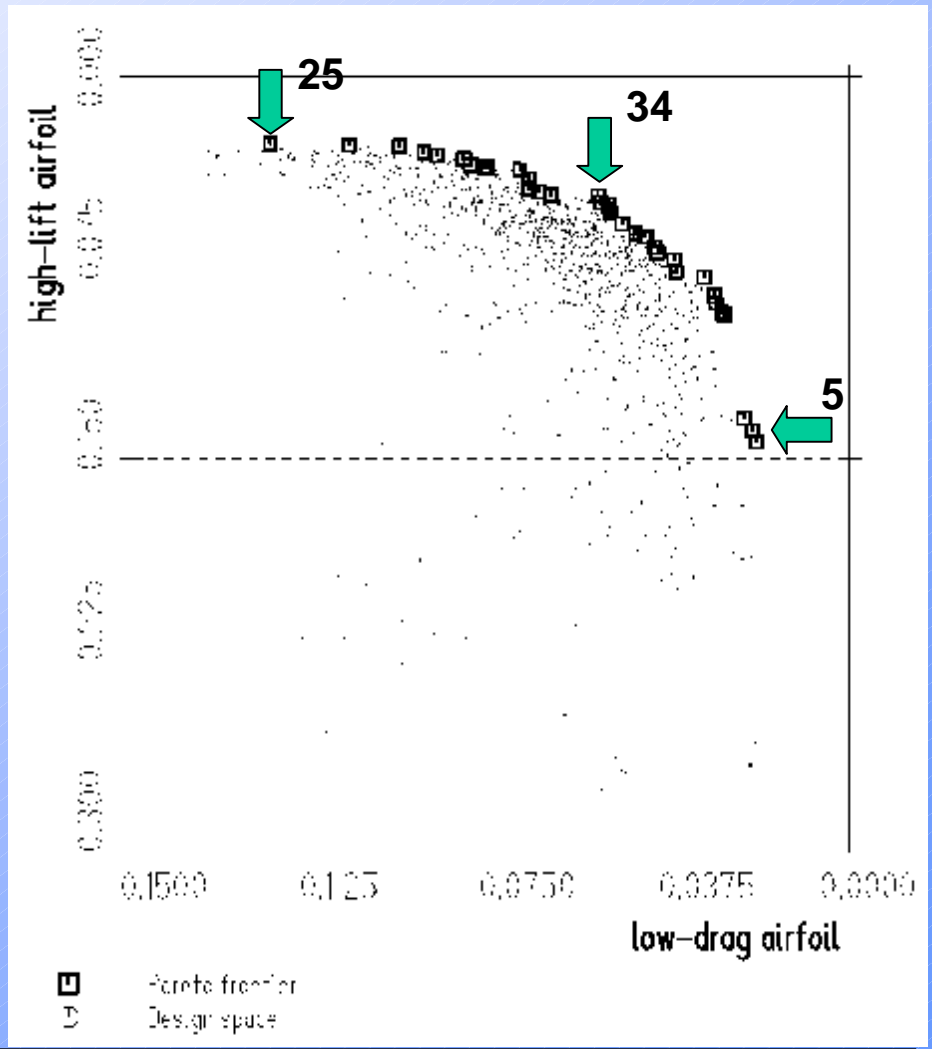
Two-point airfoil design - Pareto results

Individual 25 is the best non-dominated individual for the high lift airfoil with objective function values of:

- LD: $1.21 \cdot 10^{-1}$
- HL: $2.60 \cdot 10^{-2}$

Individual 5 denotes the best low-drag, non-dominated individual with objective function values of:

- LD: $2.03 \cdot 10^{-2}$
- HL: $1.39 \cdot 10^{-1}$



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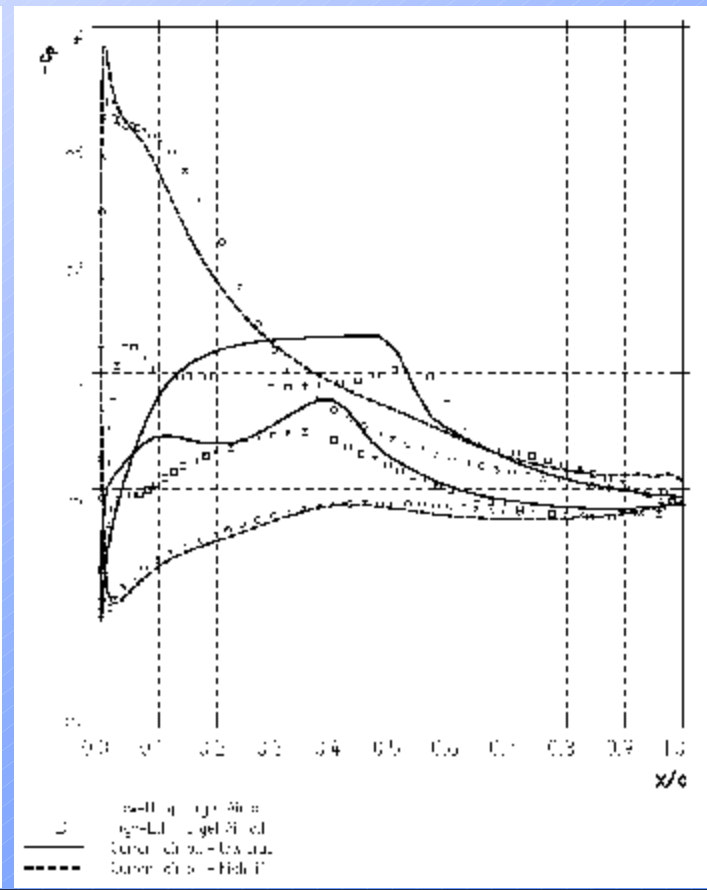
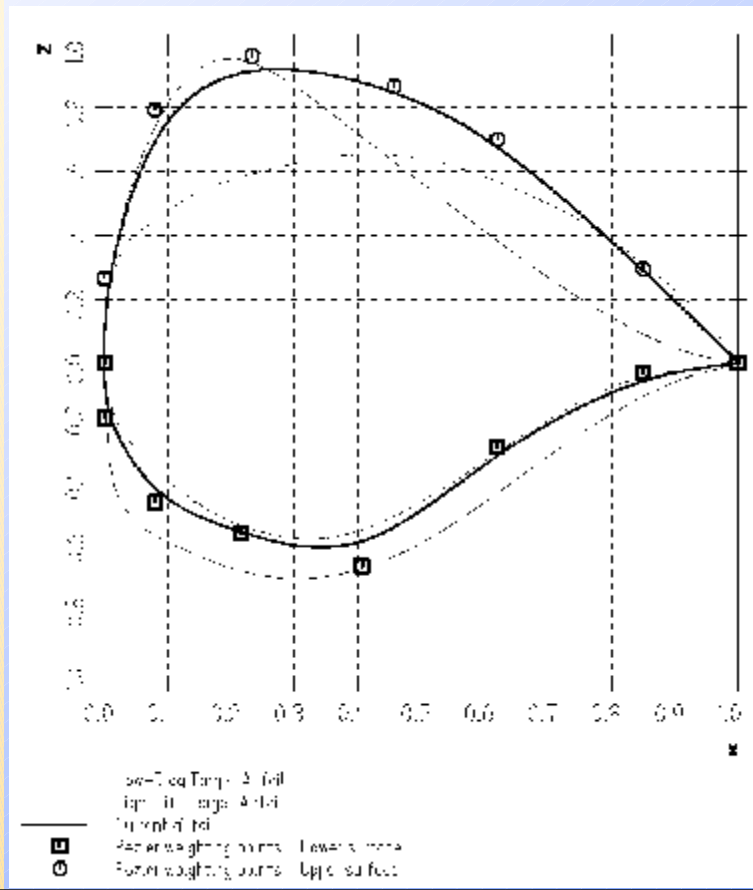
Hale - Loiter time

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Conclusions

Two-point airfoil design - „Compromise“ result

Non-dominated **individual 34** from Pareto frontier as an engineering compromise between low-drag and high-lift airfoil



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RAE2822
Drag minimisation

=

Three-point
airfoil design

Design points:

1. $M_1 = 0.734, \alpha_1 = 2.8^\circ, Re = 6.5 \times 10^6$
2. $M_2 = 0.754, \alpha_2 = 2.8^\circ, Re = 6.2 \times 10^6$
3. $M_3 = 0.680, \alpha_3 = 1.8^\circ, Re = 5.7 \times 10^6$

Objective:

$$OBJ = 2 C_d(\alpha_1, M_1) + C_d(\alpha_2, M_2) + C_d(\alpha_3, M_3)$$

Constraints:

1. $C_l(\alpha_1, M_1) \geq C_l^t(\alpha_1, M_1)$,
2. $C_m(\alpha_1, M_1) \simeq C_m^t(\alpha_1, M_1)$ - variation of $\pm 2\%$ allowed,
3. $C_l(\alpha_2, M_2) \geq C_l^t(\alpha_2, M_2)$,
4. $C_m(\alpha_2, M_2) \simeq C_m^t(\alpha_2, M_2)$ - variation of $\pm 2\%$ allowed,
5. $C_l(\alpha_3, M_3) \geq C_l^t(\alpha_3, M_3)$,
6. $C_m(\alpha_3, M_3) \simeq C_m^t(\alpha_3, M_3)$ - variation of $\pm 2\%$ allowed,
7. leading – edge – radius $\geq 0.91.e.r^t$,
8. trailing – edge – angle $\geq 0.8 t.e.a^t$,
9. thickness(5%) $\geq 0.96 th.^t(5\%)$.

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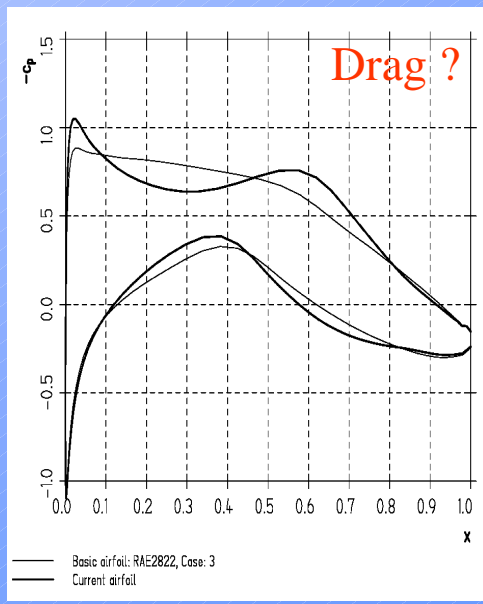
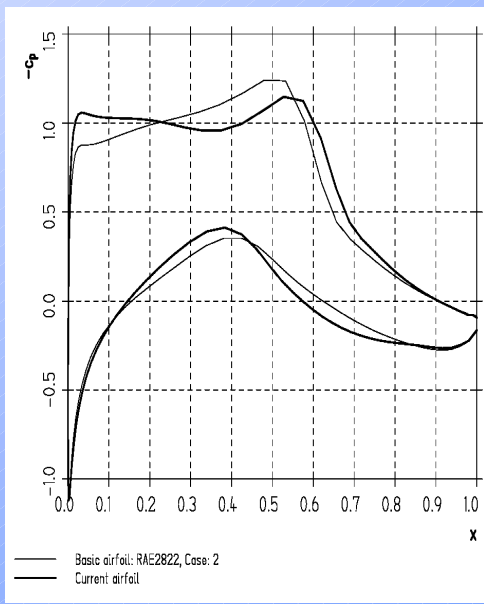
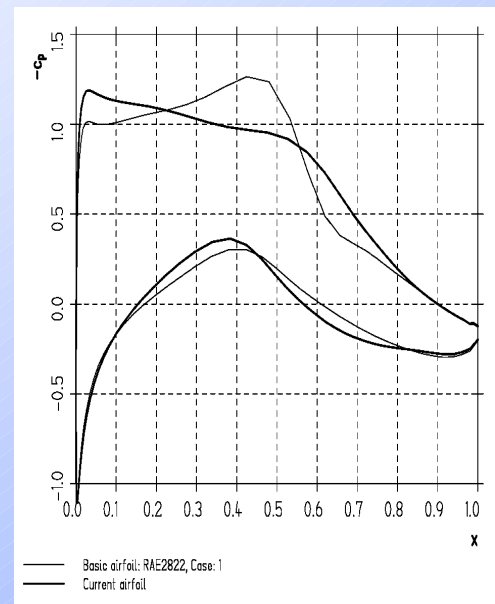
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Conclusions

RAE2822 Drag minimisation - Pressure results

*MMES (20,2,20) with 1 Objective
Coarse mesh / Design 251
Hybrid approach with NLPQLP*

Pressure distributions for optimised and initial shape for all three points



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Design network

2-point airfoil

Drag minimisation on RAE2822

SCT drag minimisation

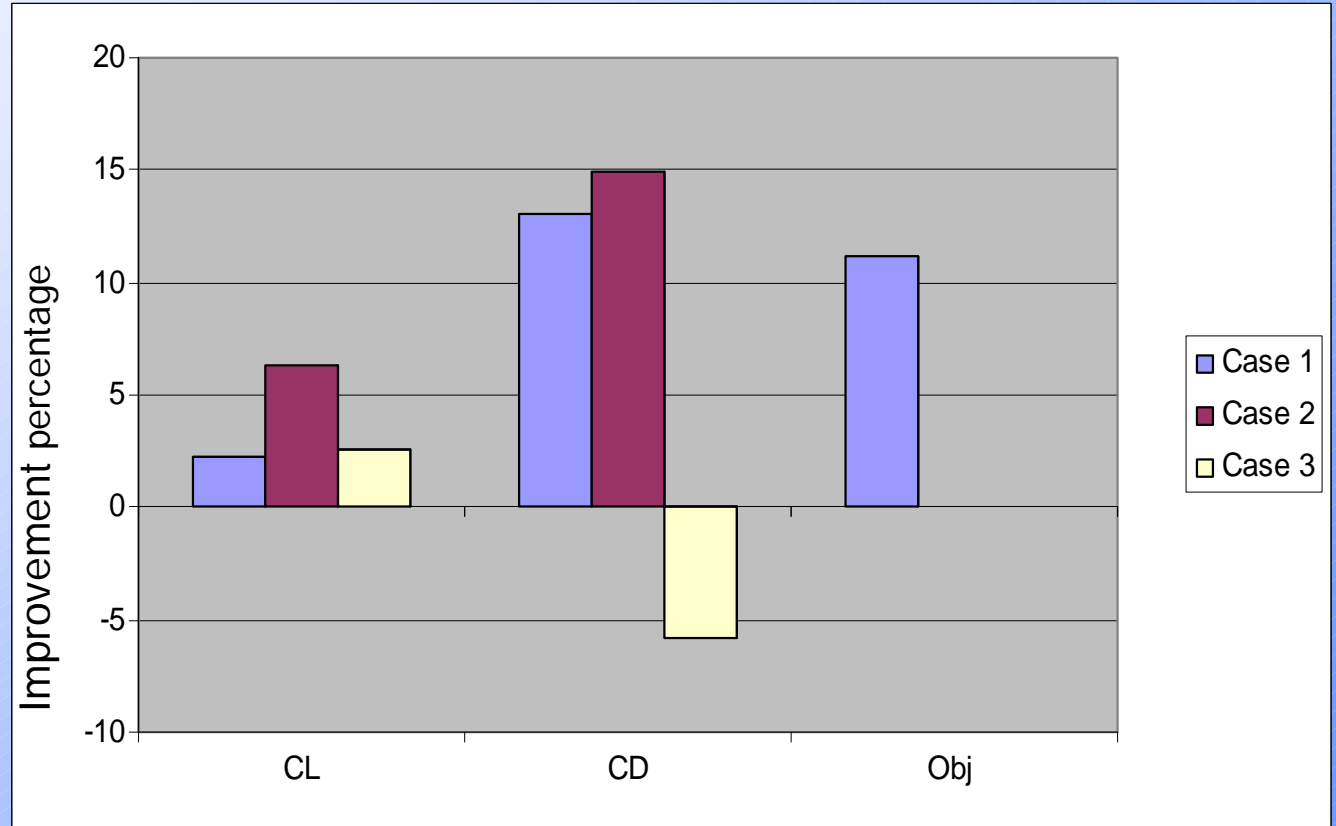
Hale – Loiter time

Robust Design

Conclusions

RAE2822 Drag minimisation - Results

*FMOGA (16,16) with 3 Objectives
Coarse mesh / Design 148*



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Design network

2-point airfoil

Drag minimisation on RAE2822

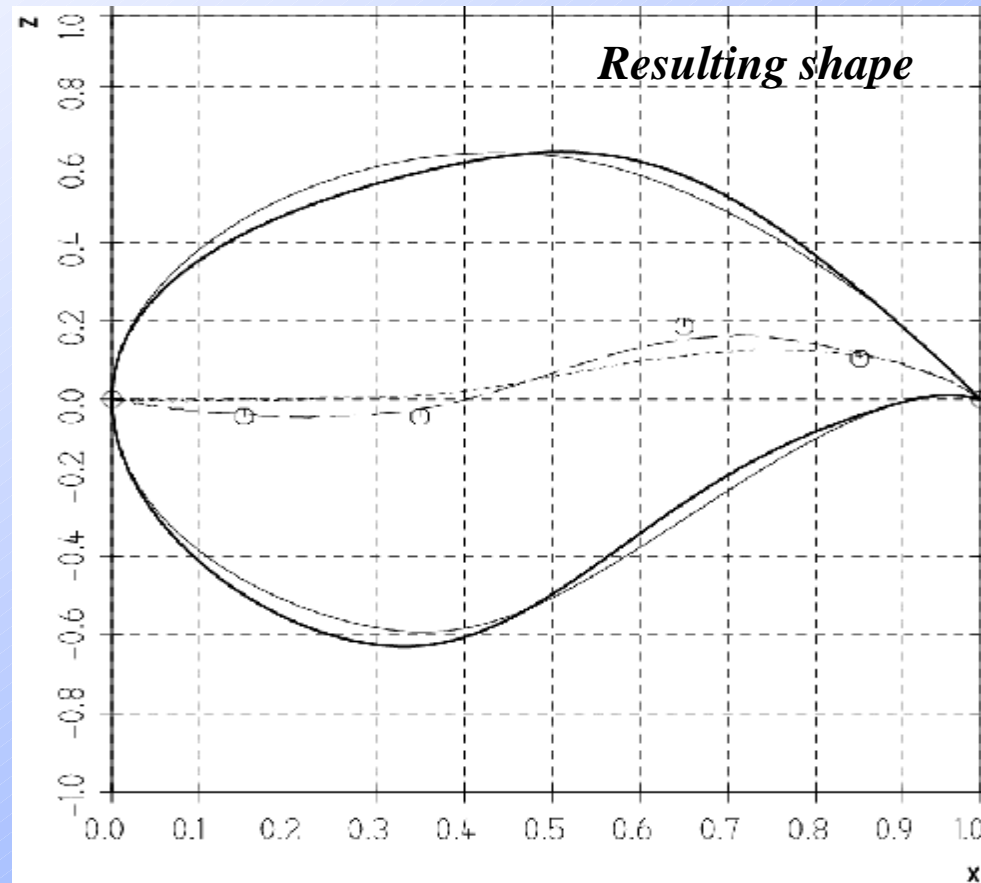
SCT drag minimisation

Hale – Loiter time

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Conclusions

RAE2822 Drag minimisation - Results



$C_m(\alpha_1, M_1) \simeq C_m^t(\alpha_1, M_1)$ - variation of $\pm 2\%$ allowed

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Supersonic Commercial Aircraft - Drag minimisation



Design network

2-point airfoil

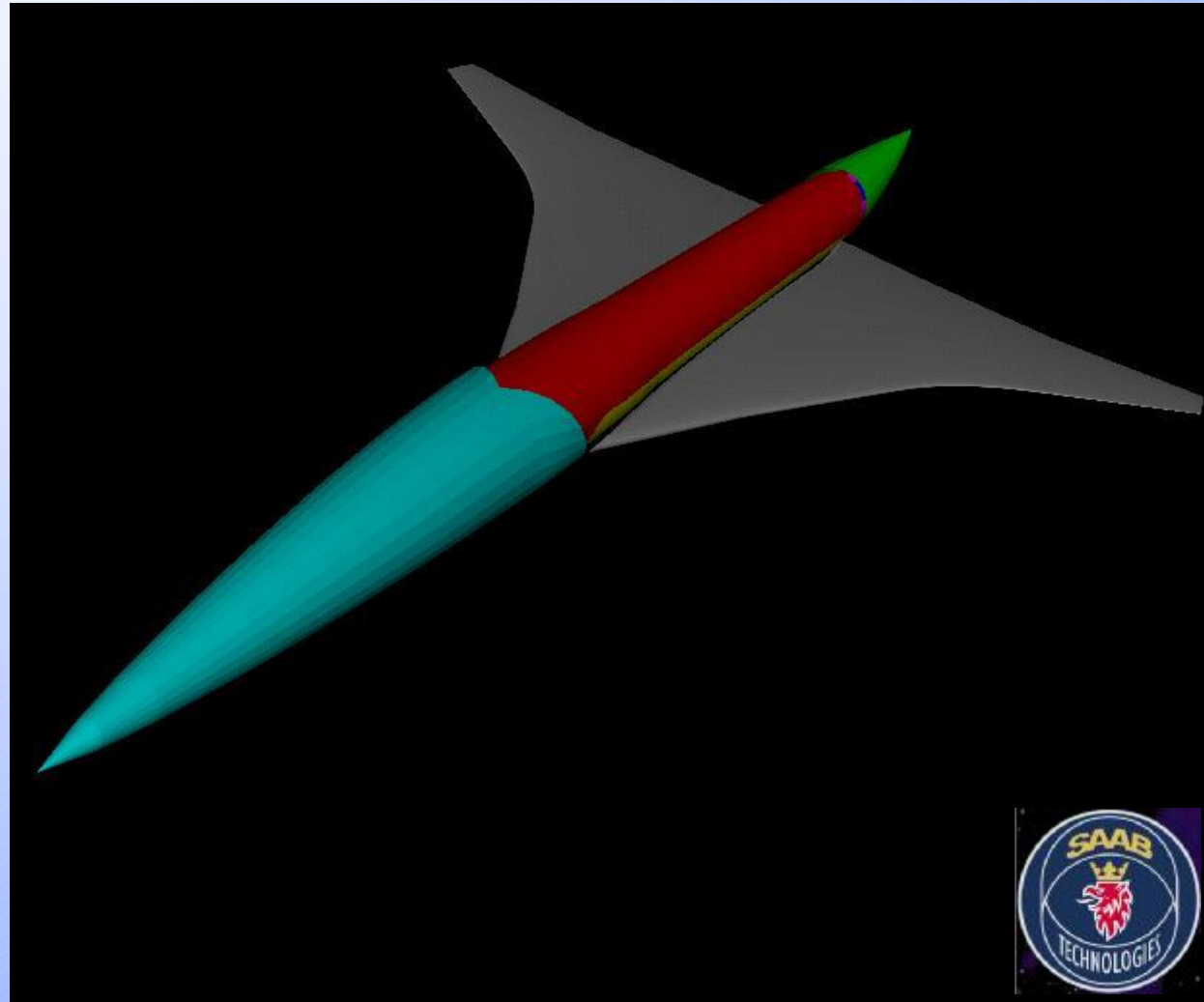
Drag minimisation
on RAE2822

**SCT drag
minimisation**

Hale – Loiter time

Robust Design

Conclusions





Supersonic Commercial Aircraft - Test case definition

Design network

M=2.0, free angle of attack, Euler solution

2-point airfoil

Parameterisation with ICEM's COMAK tool
Coupled to ICEM HEXA for grid generation

Drag minimisation
on RAE2822

Objective

Minimum drag

**SCT drag
minimisation**

Design parameters

Defining fuselage contraction, angle of attack,
asymmetric wing profiles at four spanwise positions,
twist at four spanwise positions,
25 parameters in total

Hale – Loiter time

Constraints

Pitching moment coeff. (about -0.029),
location and range of fuselage contraction,
minimum fuselage radius,
minimum of wing spanwise profile thickness
distribution, and a

Robust Design

lift coefficient = 0.12 - to be kept in the range of 10^{-4}

Conclusions

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Supersonic Commercial Aircraft - Convergence and objective space



Design network

2-point airfoil

Drag minimisation
on RAE2822

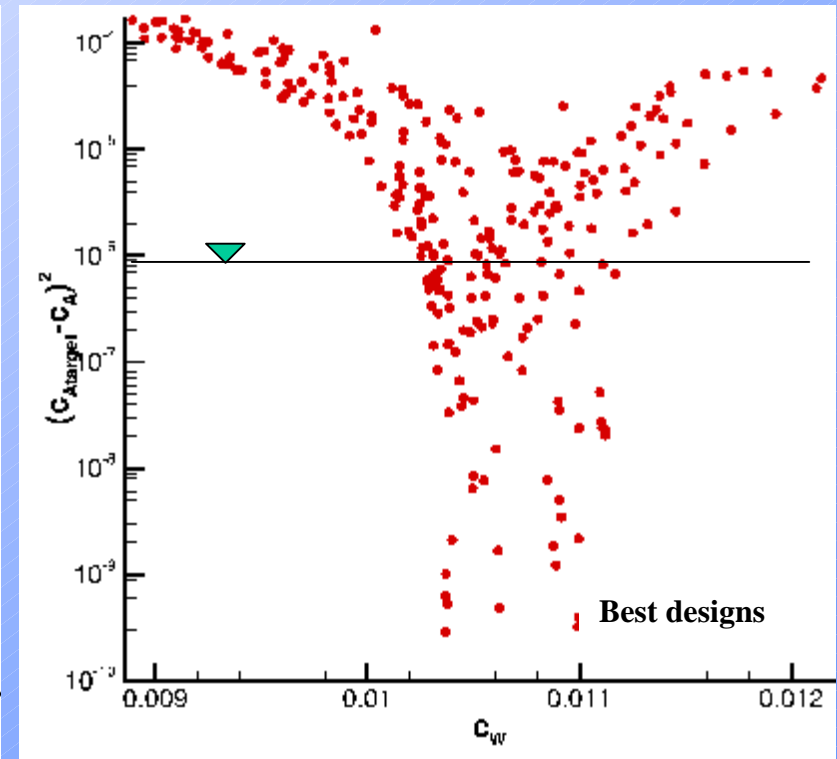
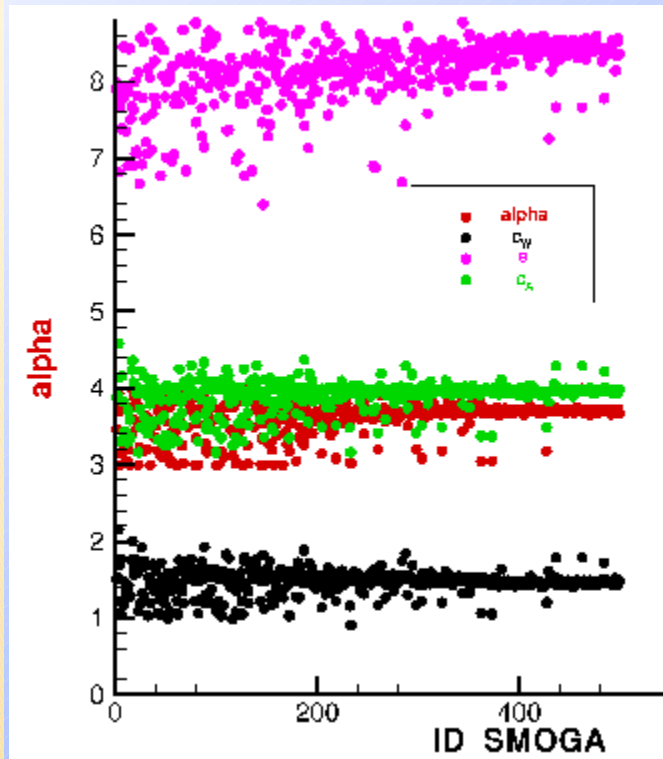
SCT drag
minimisation

Hale - Loiter time

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Conclusions

Initial population: $\mu = 50$
Number of generations: $T = 10$





Design network

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Drag minimisation
on RAE2822

**SCT drag
minimisation**

Hale – Loiter time

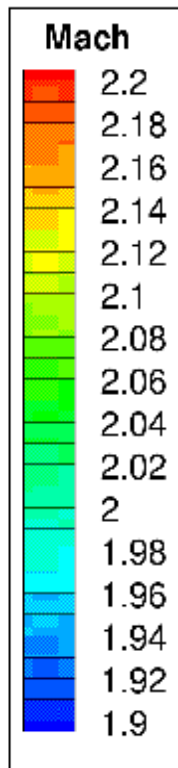
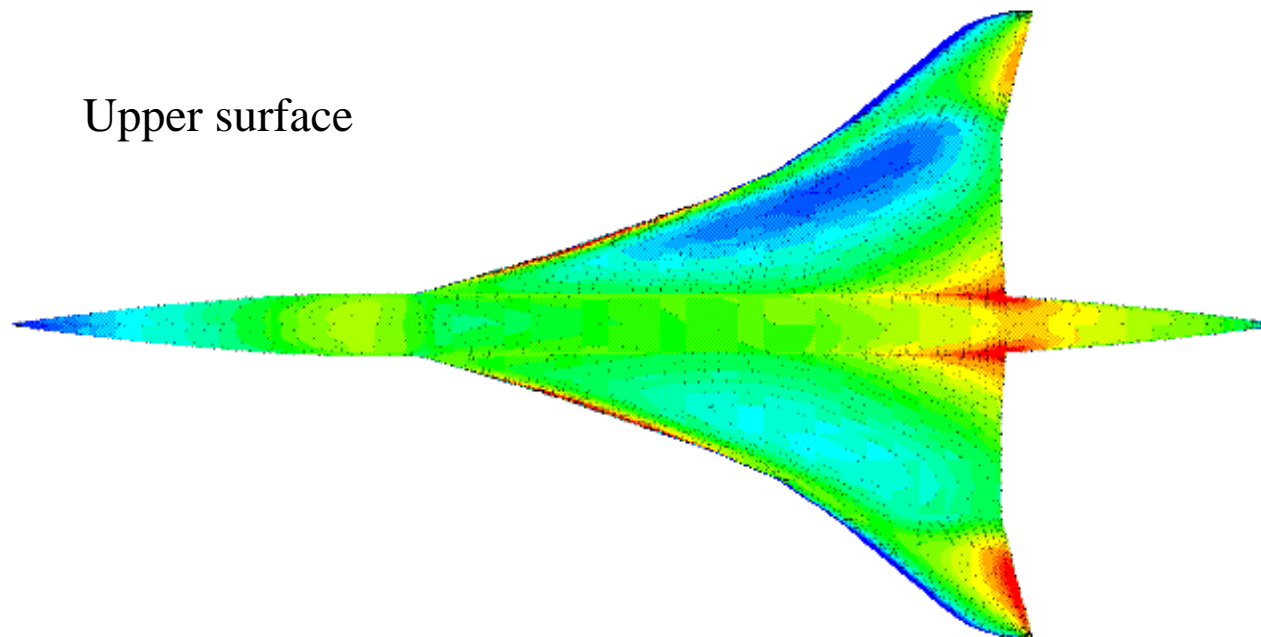
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Conclusions

Supersonic Commercial Aircraft - Baseline & Optimum

Baseline geometry, $\alpha=3.657^\circ$, medium mesh, $cl=0.1200$

Upper surface



Optimised geometry, $\alpha=3.494^\circ$, medium mesh, $cl=0.1147$

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SCT drag minimisation

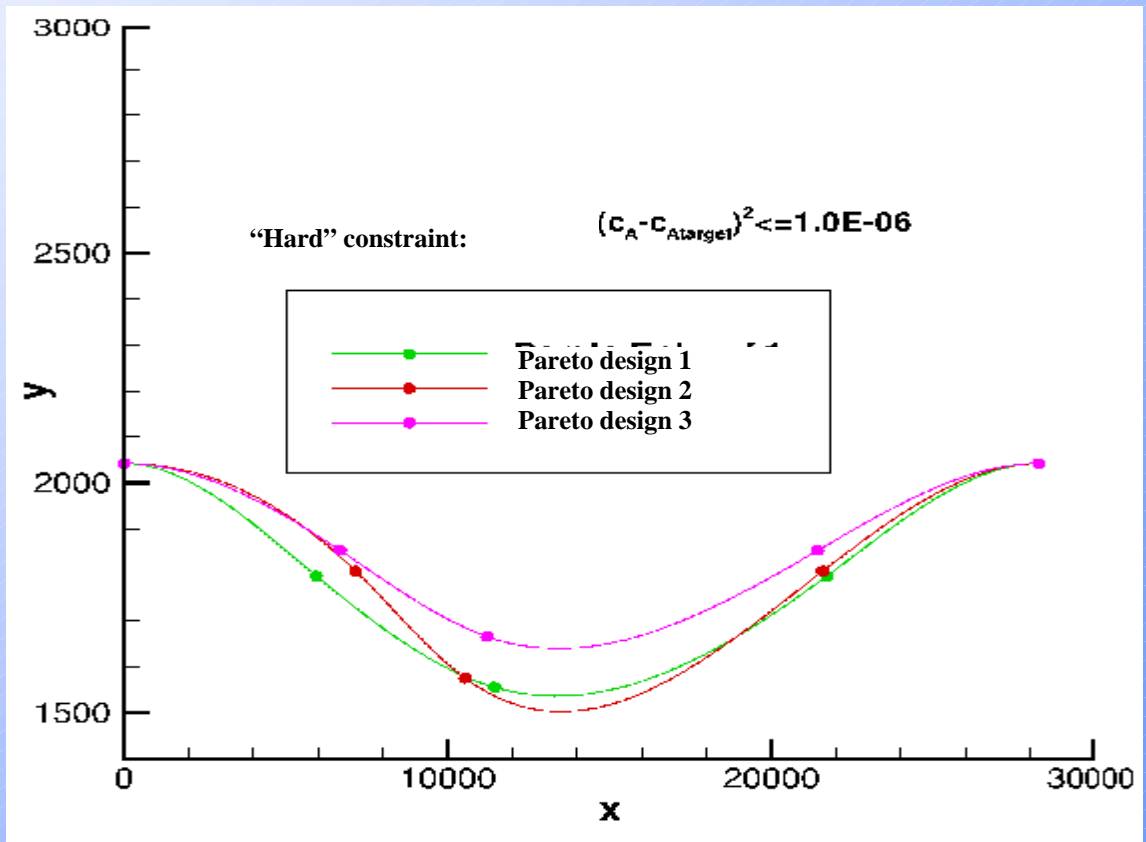
Hale – Loiter time

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Supersonic Commercial Aircraft

Fuselage contractions, Optimiser SMOGA



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Supersonic Commercial Aircraft - Mesh and solution

Design network

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Drag minimisation on RAE2822

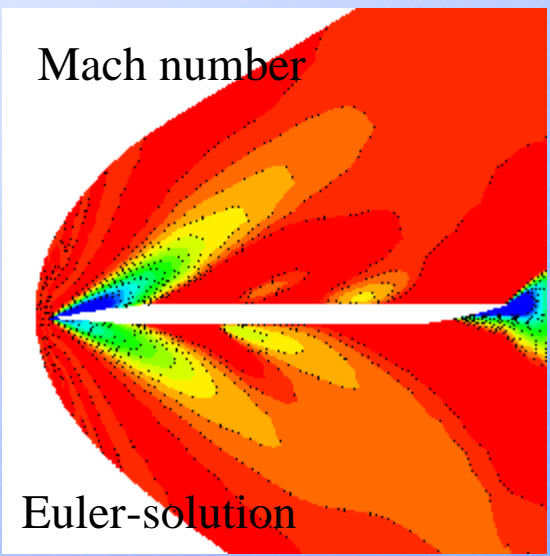
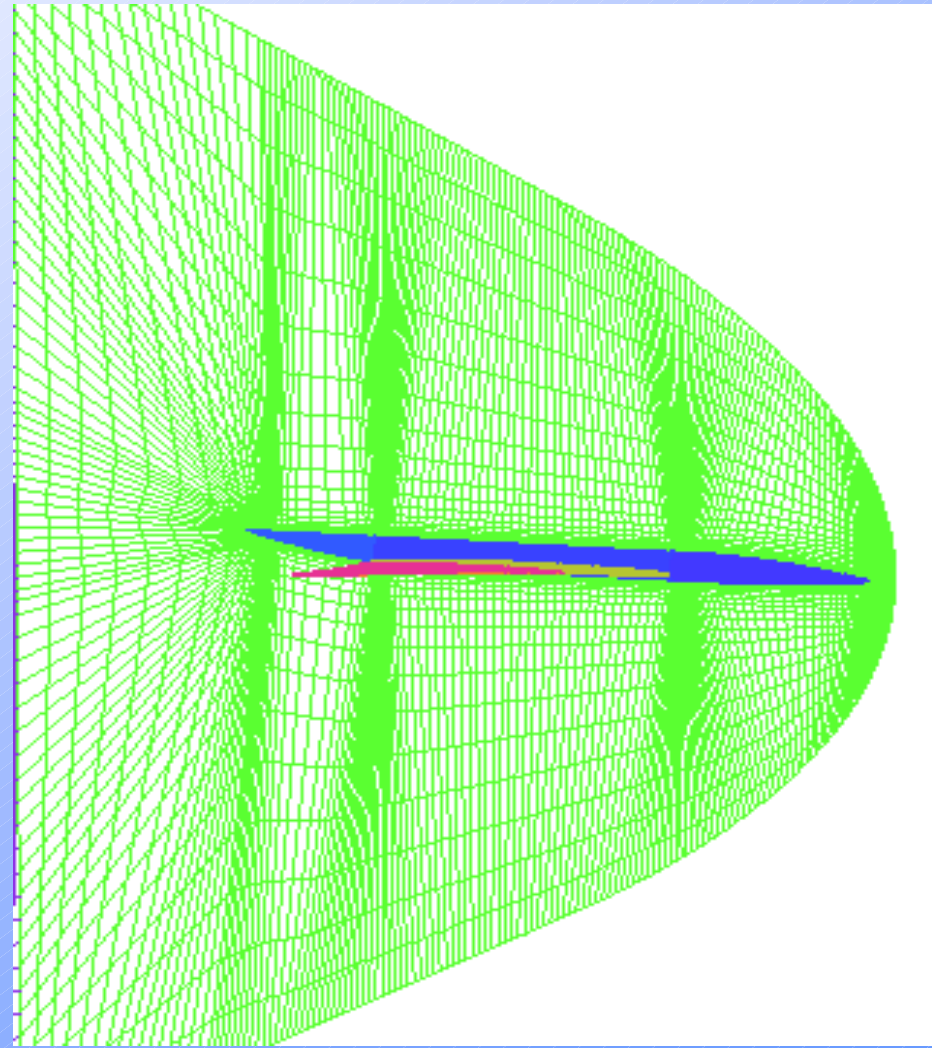
SCT drag minimisation

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Conclusions

“Fine” grid with 617,000 grid points



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Design network

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Drag minimisation
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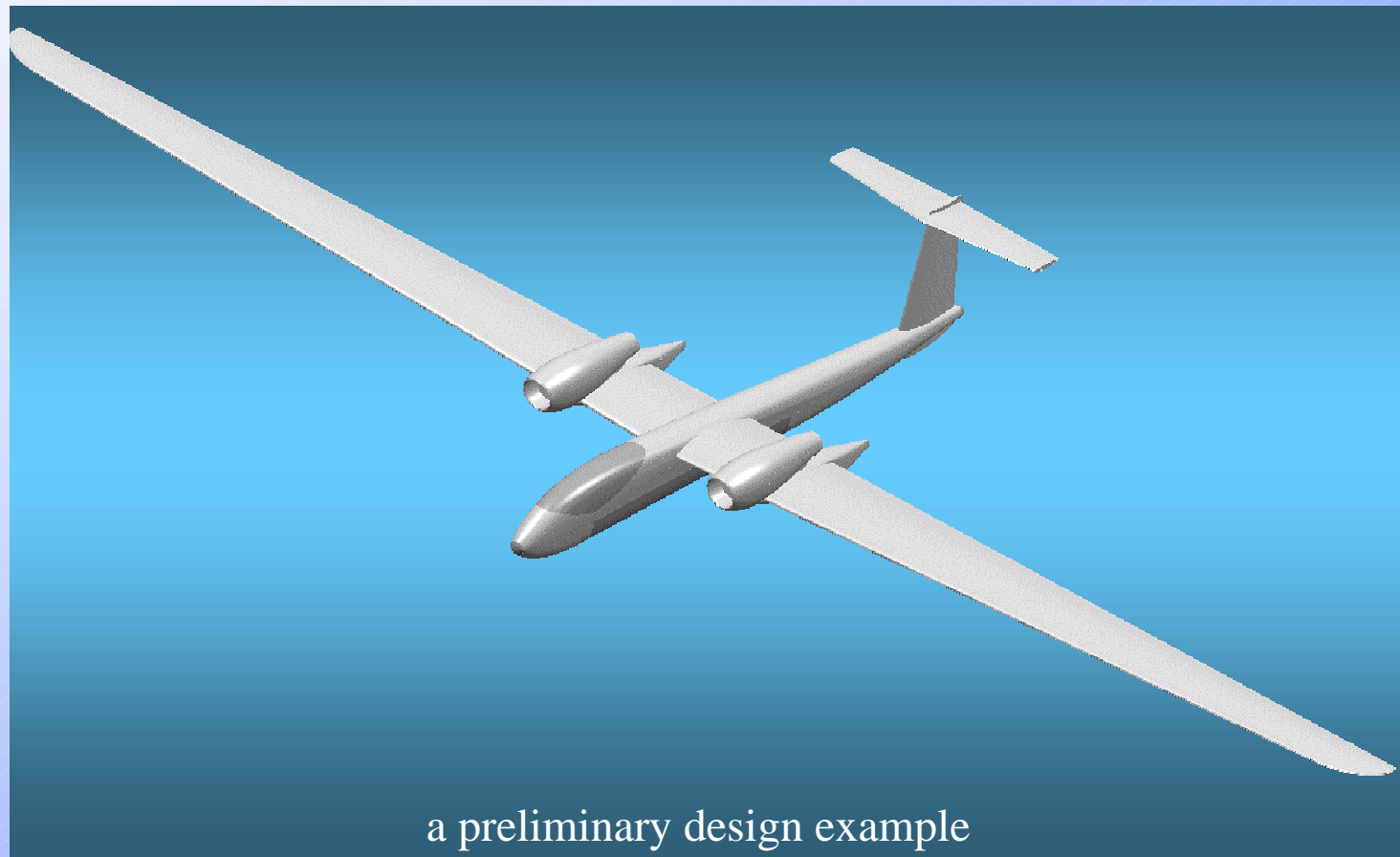
SCT drag
minimisation

Hale – Loiter time

Robust Design

Conclusions

Optimisation of loiter-time for a „Hale“ A/C





Design network

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Hale – Loiter time

Robust Design

Conclusions

Optimisation of loiter-time for „Hale“

Task/Objective

Computation of **maximum loiter time** as a function of wing-chord, profile thickness, Mach number, wing weight and the resulting drag.

According to Ma, altitude, weight and Wing-area, a “design lift coefficient” is derived – from which the drag coefficient of the optimal profile (turbulent flow) is computed.

Design variables

Mach number at start of loiter

Wing area [m**2]

Relative wing thickness [-]

Altitude at start of loiter is fixed (15km and 16 km, 17 km “not met”
according to selected engine)

Wing span [m] – we have changed upper bound in different runs (!)



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Conclusions

Optimisation of loiter-time for „Hale“

Constraints

Drag < thrust for the given engine

Critical Mach number

Max. take-off weight

Max. drag: to be lower than max. thrust

Wing thickness > 0.24

Optimiser

DES (single objective ES)

[additional GA and NLPQLP runs]

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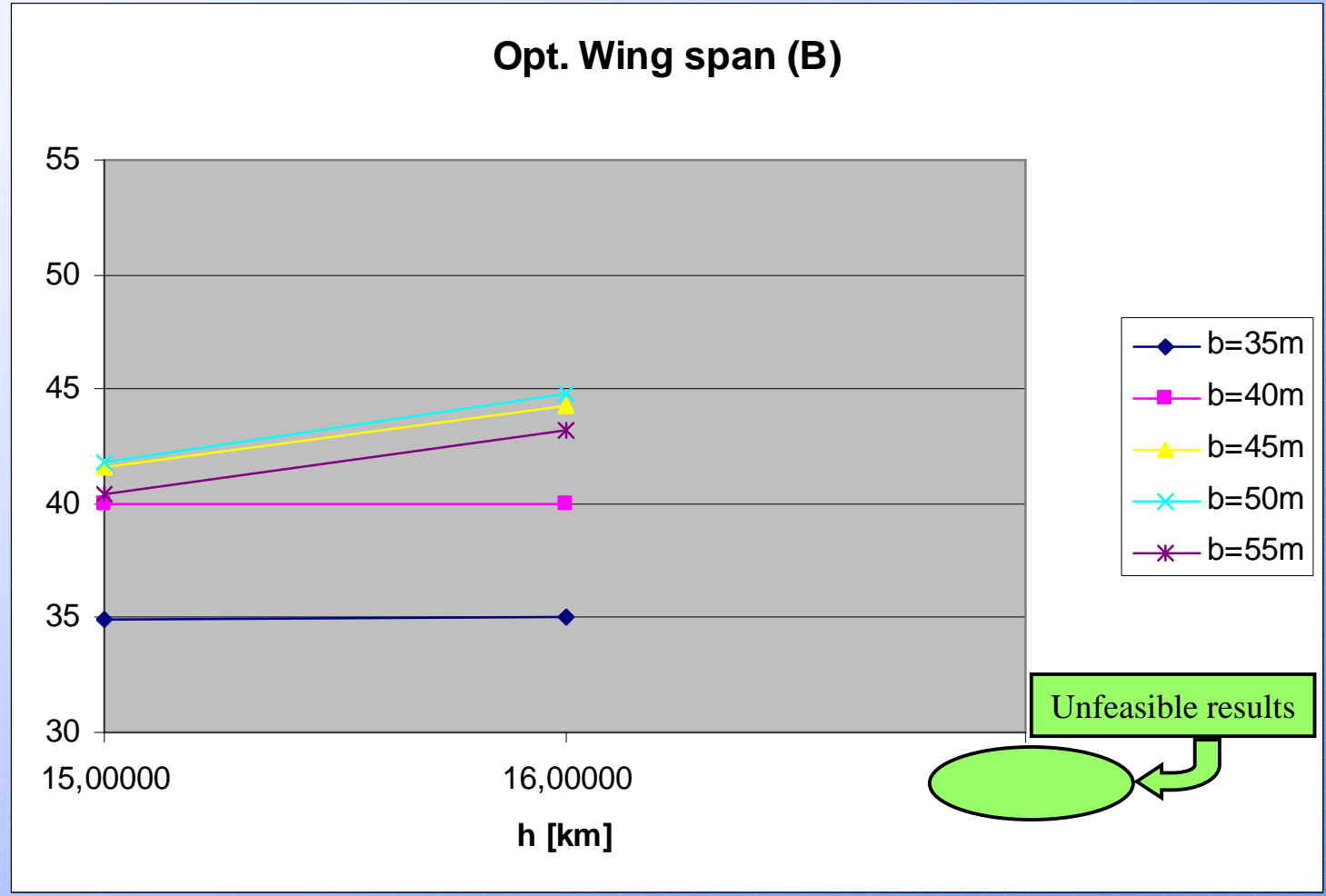
SCT drag minimisation

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Optimisation of loiter-time for „Hale“



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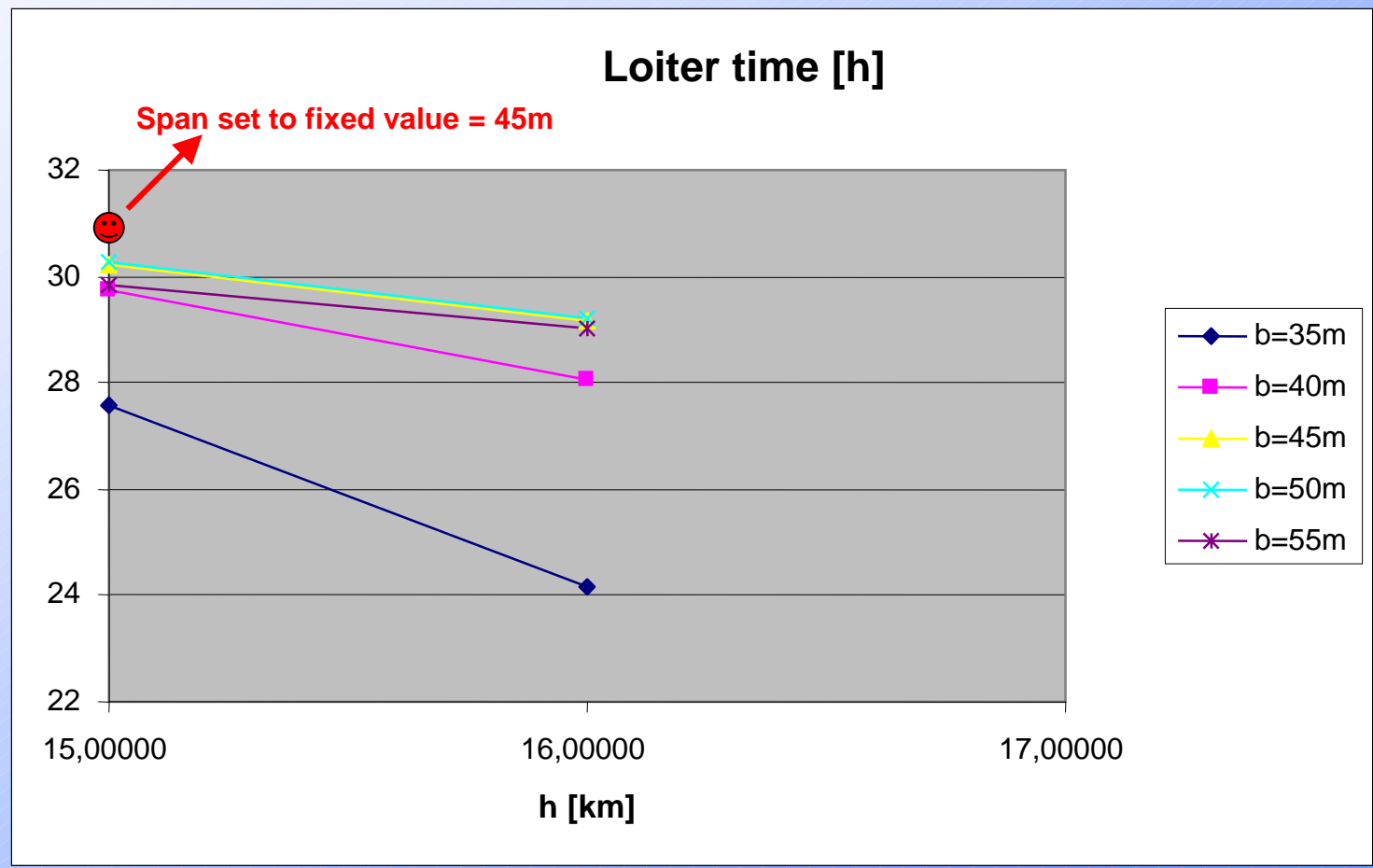
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Optimisation of loiter-time for „Hale“ Conclusions

- As mentioned, the “fixed-span” optimisation turned out to be an extremely “peaky” optimum, i.e., in the close vicinity of this design no other can be found.
- Using an NLPQLP (SQP) method resulted in completely non-feasible solutions around the $B=45\text{m}$ goal, because
- a collision between max. take-off weight and wing thickness occurred; either thickness or take-off weight were violated and small changes in the constraints gave rise to completely different solutions.
- Thus we must find another way to (maybe) reach the $B=45\text{m}$ goal – if it is then one: **Robust design**

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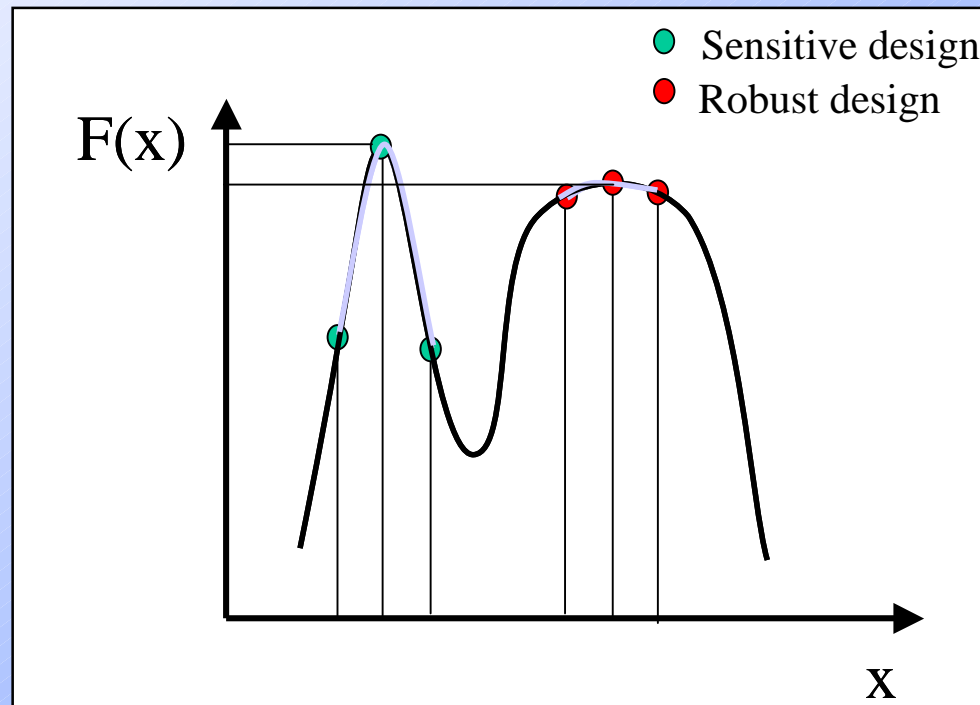
Hale – Loiter time

Robust Design

Conclusions

Robust design

- It has been seen that the **best solution is NOT identical to the best average solution** (an averaged variables distribution)
- Thus two additional objectives are to be employed:
Maximise average function inside the variables distribution and **minimise standard deviation** – leading to multi-objective optimisation



=> **Topic of
current research**

Courtesy of L. Padovan, ESTECO



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Conclusions

~~Conclusion~~

We are far from being self-satisfied and have hopefully stressed advantages and open questions in equal shares.

- What problem to optimise?
- How can a known problem be optimised?
- What parameterisation to use?
- Taking new mesh generation or mesh movement, and how does the mesh quality influence the optimum?
- Which analysis method to apply ?
- Definition of constraints correct?
- Objective functions? (combined or separate, i.e. multi-objective) (even combined objectives AND constraints)
- What optimiser to choose ?
- Robust design needed ?

