

NATIONAL TECHNICAL UNIVERSITY OF ATHENS

Parallel CFD & Optimization Unit Laboratory of Thermal Turbomachines

Robust Design

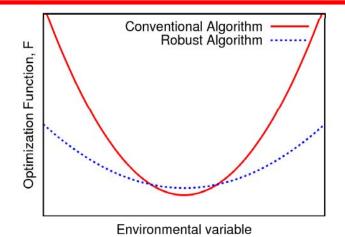
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Robust Design



(Second-Order, Second-Moment, SOSM, approach)



For N design (b_i) & M environmental (c_i) variables, minimize

 $\widehat{F} = \widehat{\mu_F} + k\widehat{\sigma_F}$

where the estimated mean and the standard deviation of F are given by

$$\hat{\mu_F} = F_{\rm D} + \frac{1}{2} \left[\frac{d^2 F}{dc_i^2} \right]_{\rm D}^{\sigma_i^2}$$

$$\hat{\sigma_F} = \sqrt{\left[\frac{dF}{dc_i}\right]_{\mathrm{D}}^2 + \frac{1}{2} \left[\frac{d^2F}{dc_i dc_j}\right]_{\mathrm{D}}^2 \sigma_i^2 \sigma_j^2}$$

$$\frac{d\widehat{F}}{db_{l}} = \underbrace{\frac{dF}{db_{l}}}_{l} + \underbrace{\frac{1}{2} \frac{d^{3}F}{dc_{i}^{2}db_{l}} \sigma_{i}^{2}}_{l} + k \underbrace{\frac{2\frac{dF}{dc_{i}} \frac{d^{2}F}{dc_{i}db_{l}} \sigma_{i}^{2} + \frac{d^{2}F}{dc_{i}db_{l}} \frac{d^{3}F}{dc_{i}dc_{j}} \frac{\sigma_{i}^{2}\sigma_{i}^{2}}{\frac{d^{2}F}{dc_{i}dc_{j}} \frac{d^{3}F}{dc_{i}dc_{j}db_{l}} \sigma_{i}^{2}\sigma_{i}^{2}}}_{2\sqrt{\left[\frac{dF}{dc_{i}}\right]^{2} \sigma_{i}^{2} + \frac{1}{2} \left[\frac{d^{2}F}{dc_{i}dc_{j}}\right]^{2} \sigma_{i}^{2}\sigma_{j}^{2}}}$$

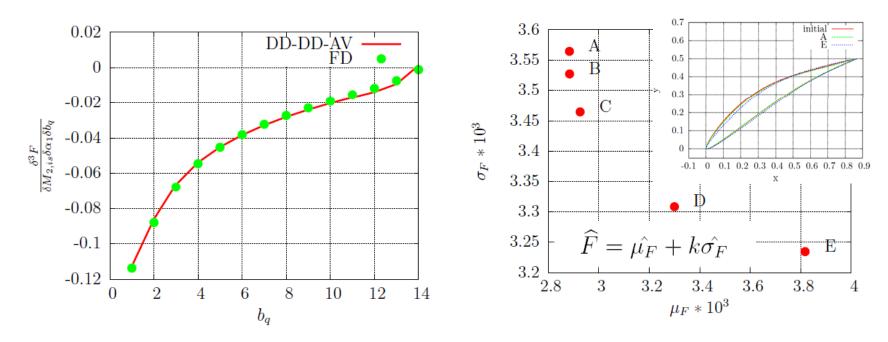
► The recommended approach, if M<<N,

 $DD_c-DD_c-AV_b$

exists and has been programmed in both discrete and continuous adjoint.

Robust Design





Robust design of a compressor cascade: Two environmental variables: $M_{2,is}$ and α_1 .

E.M. PAPOUTSIS-KIACHAGIAS, D.I. PAPADIMITRIOU, K.C. GIANNAKOGLOU: 'Robust Design in Aerodynamics using 3rd-Order Sensitivity Analysis based on Discrete Adjoint. Application to Quasi-1D Flows', International Journal for Numerical Methods in Fluids, Vol. 69, No. 3, pp. 691-709, 2012. E.M. PAPOUTSIS-KIACHAGIAS, D.I. PAPADIMITRIOU, K.C. GIANNAKOGLOU: Discrete and Continuous Adjoint Methods in Aerodynamic Robust Design problems, CFD and Optimization 2011, ECCOMAS Thematic Conference, Antalya, Turkey, May 23-25, 2011.